

Superconductivity & Particle Accelerators conference 2024

Progress in technological solutions for EU-DEMO magnets advanced conductors

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EUROfusion Consortium:

supports and funds fusion research activities to pave the way for fusion power reactors. Consortium done by 31 European Research Units + 162 Affiliated Entities

Magnet System Work Package:

Design and develop technology for EU-DEMO Magnets

WPMAG members (~ 80 people):

CEA (France), CU (Slovakia), **ENEA (Italy)**, EPFL (Switzerland), FOM-DIFFER (Netherlands), IAP (Romania), IPP.CR (Czech Republic), IPPLM (Poland), KIT (Germany), OEAW (Austria), VTT (Finland)





Introduction on EU DEMO tokamak

Quench Experiment on sub-scale HTS samples

Design and R&D on Full-scale HTS conductors

Conclusions



EU-DEMO reactor is designed for demonstrating net production of electricity and operation with a closed fuel cycle (TBR>1)



16 TF coils (B_{peak}= 12T, E_{total} = 150GJ)

5 CS coils (B_{peak}= 15.8 T, E_{total} = 15GJ)

6 PF coils (B_{peak}= 8 T, E_{total} = 21GJ)

Parameters	Symbol	EU-DEMO	
Major radius	R ₀ (m)	9	
Minor radius	a (m)	2.9	
Aspect ratio	Α	3.1	
Plasma current	lp (MA)	18	
Safety factor	q	3.6	
Plasma elongation	k ₉₅	1.6	
Triangularity	δ ₉₅	0.33	
Av. electron density	<n<sub>e,vol> (10²⁰m⁻³)</n<sub>	0.73	
Eff. ionic charge	Z _{eff}	2.2	
Confinement enhancement	н	1.1	
Burn Time	t _{burn} (hrs)	2	
Bootstrap fraction	f _{bs} (%)	37	
Fusion Power	P _{fus} (MW)	2000	
Net electric power	P _{e,net} (MW)	500	
Divertor configuration		Single null	



DEMO CS WP: Hybrid variant

Design		Hybrid variant		
Total current [MAt]		72.2		
Cond current [kA]		46.3		
R _i [mm]		1520		
R _o [mm]		2700		
Max B [T]		15.8		
Mag flux [Wb]	Only CS	218.5		
	CS+PF	239		
σ _{hoop} [MPa]		295.4		

5 modules CS (with a central double one)

- The hybrid variant allows the Increase of the magnetic flux wrt the ITER-like design of 13%.
- Layer winding with grading on superconductor and stainless-steel



Need to study HTS conductors suitable for the EU-DEMO central solenoid

Experimental activity on HTS conductors

Experiment to study the quench propagation on sub-scale (15 kA) HTS conductors.

Motivation: quantify the slow propagation velocity of the hot spot after a quench (compared to LTS conductors), which may require a change in the quench detection approach.









Conductors based on stacks of REBCO tapes

Inlet Temperature = 4.5 K DEMO Peak field = **18 T** CS target Operating current = 60 kA Minimum bending radius = **1.5 m**

Assess the performance of full-scale HTS conductors with electromagnetic cycles **Motivation:** Trying to reduce the degradation of the

performances with cyclic electromagnetic loads in full-scale HTS conductors.



ASTRA

SECAS





Quench Experiment



Quench test: Al slotted core sample

A: 4 stacks x 19 HTS tapes (76 SuperOx Tapes - No APC tapes)

- 6-slot Al-core;
- Straight slots/straight stacks
- double jacket concept (inner Al and outer SS)

SULTAN sample





Performance analysis of the conductor: I_c test





Quench tests @ 10.85 T, 15 kA

Quench tests:

- direct power supply keeps the current constant
- quench is induced by heating the He at the inlet
- current is dumped when a T threshold is reached



Protruding sensors in HFZ @ T₂*, T₃*, T₄*

Ty 2

Ty_1

Tz

Quench tests – degradation after T_{hot spot} = 200 K



 $I_c = 8.9 \text{ kA} \rightarrow 10\%$ reduction between test before and after QE tests



Quench Experiments: comparison with previously tested samples

Conductor	Stabilizer	Stabilizer cross section (mm²)	J _{stabilizer} (A/mm²)	I _{op} (kA)	Steel cross section (mm ²)	Design and manufacture
Reference (twisted)	Cu	150	100	15	715	SPC
Non-twisted	Cu	150	100	15	715	SPC
Solder-filled (Bi ₅₇ Sn ₄₂ Ag ₁ solder)	Cu	150	100	15	652	SPC
Aluminum Slotted Core	AI	180 +12 (Cu in the tape)	83	15	81	ENEA

N. Bykovskiy, SUST 36 (2023) 034002

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O. Dicuonzo 2022 PhD Thesis (http://infoscience.epfl.ch /record/293510)

Quench Experiment: Normal Zone Propagation Velocity

Mark time at which $E > E_{threshold}$, knowing distance L between taps \rightarrow Normal Zone Propagation Velocity (NZPV) = L/(t₂-t₁)





Ethreshold = 1 mV/cm: high enough to exclude sensors noise. At 1 mV/cm Ic~100 A (at about 70 K) -> all current is flowing in Cu A. Zappatore, Cryogenics 132 (2023) 103695



□ In reference conductor: largest temperature differences in the cross-section

□ In solder-filled: smaller temperature differences, slowest temperature rise

□ In Al slotted core: faster evolution, smaller temperature differences. Measured T_{stack} very close to T_{hotspot} that is reconstructed from voltage:

$$\Delta V_{q} = L \frac{\rho_{e,stabilizer}(\mathbf{T_{hotspot}})}{A_{stabilizer}} \cdot I_{tot}$$



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Quench Experiments: comments

- In ENEA conductor the sample degraded after T_{stack} =200 K was reached, likely because of thermal gradients.
 - **ENEA conductor and solder-filled conductor** guarantee a **better thermal contact** among their sub-elements $\rightarrow \Delta T_{max} \sim 35-40$ K in the cross-section; in reference and not-twisted conductors, point-contact between copper profile and jacket leads to $\Delta T_{max} > 100$ K in the cross-section.
- NZPV in range 10-50 mm/s, i.e., 1-2 orders of magnitude smaller than in LTS (ITER conductors)
- Smaller NZPV in solder filled due to larger heat capacity wrt the other conductors.



Full-scale HTS conductors

16 Valentina Corato | SPAS 2024 - Cracow | October 22, 2024



<u>Aligned Stacks Transposed in Roebel Arrangement (ASTRA)</u>





- 3.3 mm SST tapes, 21-tape soldered stacks
- 6 transposed strands (L~0.75 m) \rightarrow reduce AC losses
- Aqueous DMSO (Dimethyl Sulfoxide) impregnation (for mechanical support)
- Tight cooling channel \rightarrow conduction cooling
- Operation in parallel background magnetic field → reduce # tapes

ASTRA Conductor prototype: test results







- Initial DC performance in-line with expectations both from LN2 bath and SULTAN testing.
- Strong performance reduction by EM load (at 9 T, 63 kA ~570 kN/m) and thermal stresses by frozen aqueous DMSO due to its thermal expansion
- Voids and pores in soldered stack might be the root cause, thus strand manufacturing is being revised trying either to improve soldering or avoid using it (using BRAST strands).



SECAS conductor development



BRAided STAcks **(BRAST)** of REBCO tapes

High-current / high- field SECtor ASsembled (SECAS) CICC



BRAST Features

Flexible Compact Easy to handle





Non-monolithic structure of the stabilizer → limited AC losses?



BRAST mechanical assessment: twisting and compaction





Core: Cu tube, dia. 38 mm, with machined spiral slot (Twist Pitch 1.2 m) HTS strand: <u>BRAST</u> 10 tapes (SuperOx Jp, 12 mm x 0.08 um), <u>Braid</u>: 144 Cu wires, dia. 0.15 mm Jacket: Circle-in-square SS tube (PF ITER cable), 54 x 54 mm, compacted with a 4 rolls mill @CRIOTEC Impianti (Italy)



SECAS sub-cable: electric performances

In line with calculated cable critical current by FEM model

De Marzi, et al., SuST 34 (2021)



Sample TEST in LN2 @ the ENEA 20kA test facility





BRAST#3 has been **BENT** to **R** = **1.5 m** (as required for the **EU-DEMO CS** coil winding)

BRAST #3 bending to target R = 1.5 m

BRAST #3 in BENT configuration



BRAST#3: Test on BENT Conductor

A limited (5%) reduction in I_c is observed on the bent sample compared to the straight one.







Conclusions

- The performance of ENEA Al-slotted core sample is in agreement with predictions and is stable.
 BUT I_c degradation by 10 % @ 10.85 T, 15 K occurred after the sample reached T_{hot spot} > 200K
- 2) Despite the different configurations the NZPV is in range 10-50 mm/s, i.e., 1-2 orders of magnitude smaller than in LTS (ITER conductors)

Full-scale conductor characterization

□ All HTS conductor prototypes have initial performances in line with expectations

□ ASTRA conductor: degradation of the performances due to voids and pores in soldered stacks

SECAS conductor: full-size design is complete, the manufacture is in progress. SULTAN test in 2025. The subsize sample performances are as expected. Under bending, a limited (5%) reduction in I_c is observed.

Thanks for your attention!



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Increasing hotspot temperatures \rightarrow evolution of the *E*-*T* curves in HFZ



E-T curves shift after first QE with $T_{hotspot} = 45$ K After QE @ $T_{hotspot} = 205$ K \rightarrow larger shift

> (*) Fit $E = E_0 + E_c (T/T_{cs})^m$ provide similar Tcs, *m*-index

Increase in bottom joint R could determine a different fraction of current on Al/SS stabilizer \rightarrow inducing larger *E*field offset in *E*-*T* measurements

Effect on T_{cs} @ 15 kA, 10.85 T not detectable (possibly masked by this increase in E-field offset)

BRAST#3: First tests on BENT Conductor



Transition occurs at
 20% lower current than
 in Straight sample

- BUT transition occurs at termination B
 - Evident Current
 transfer phenomena
 between tape stack and
 the other components
 in the cross-section.

Re-assembly of BRAST#3 termination

- Termination (partially) dismantled and re-assembled;

- A split coil (**B**_{max} = **100 mT**) added, in the attempt to «force» the transition to occur at the center.





Pre-tinned and soldered



BRAST#3: Final tests on BENT Conductor



A limited (5%) reduction in I_c is observed on the bent sample compared to the straight one.

- Transition shifts to higher current values.
- Transition occurs most likely at the center.
- Transition measured over terminations is very similar to the one measured over the stack.

